

A photograph of a construction site. In the foreground, a large roll of white geotextile fabric is being unrolled on the ground. Two workers in safety vests and hard hats are visible. In the background, there are large piles of earth and a yellow excavator. The sky is overcast.

FHWA GeoGauge Workshop

29 & 30 November, 2000

Background & Theory

Why The GeoGauge?

- **To Meet A Need**
 - Relentless Pursuit of Lower Cost & Higher Quality
- **By Achieving A Goal**
 - Increased Precision of Design & Construction
 - Mechanistic Designs
 - Performance Specifications
 - Process Control
 - Increased Continuity Between Design & Construction
 - Design Parameters Used to Evaluate Construction
 - Contractor Warranties
- **Through A Historically Successful Path**
 - Structural Stiffness & Material Modulus

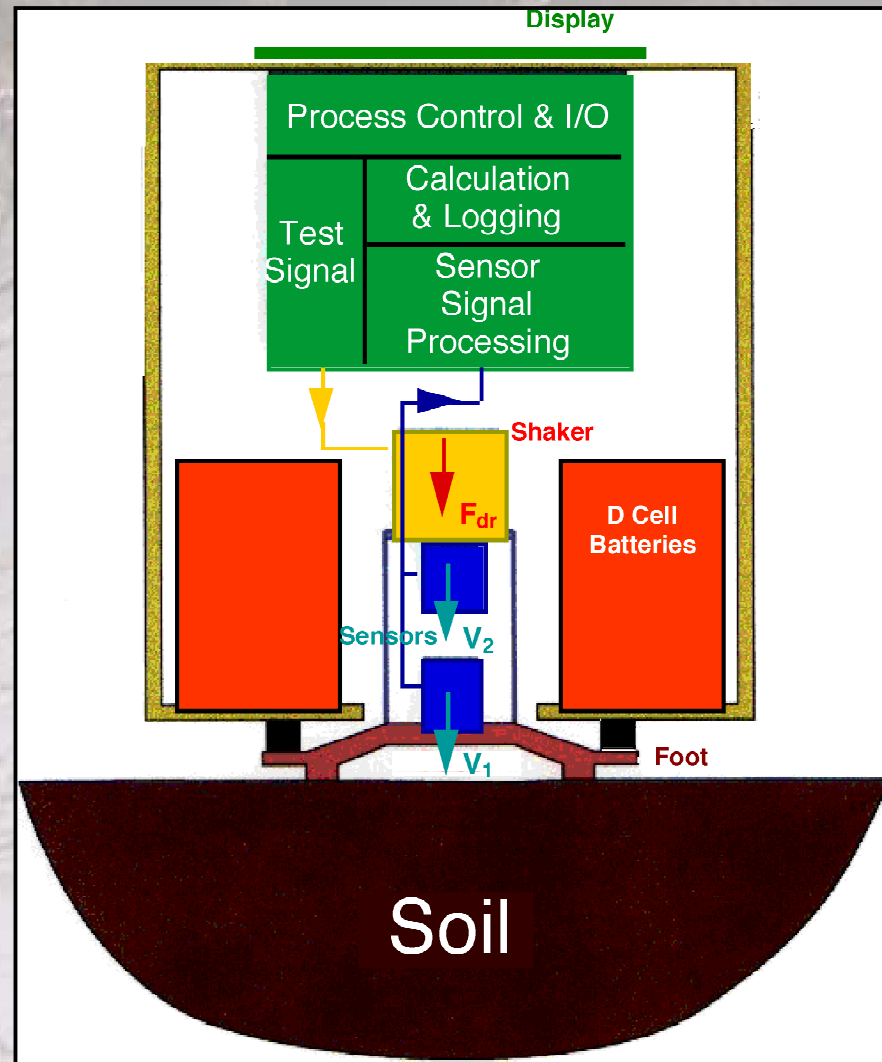
A background image of a construction site. In the foreground, a worker in a white hard hat and orange safety vest stands on the left. In the center, another worker in a white shirt and orange vest is looking down. In the background, a yellow excavator is visible, along with large mounds of earth and utility poles under a cloudy sky.

Design Description

Physical Attributes
Principle of Operation
Operating Procedure
Performance
Alternatives

Physical Attributes

- Size: 11" OD x 10" tall
- 4.5" OD x 3.5" ID Foot
- Weight: 22 lb.
- Powered by 6 D-Cell Batteries
- IR Data Downloading
- Keypad User Interface



Operating Principle

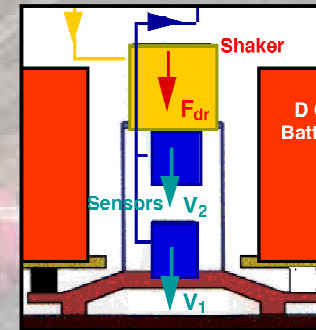
Stiffness

Resistance of a Lift to Deformation

Foot Radius & Poisson's Ratio

Modulus

Resistance of a Material to Deformation



- At GeoGauge Frequencies & Stress, Impedance is Predominately Stiffness
- No Need for a Non-moving Displacement Reference
- Permits the Accurate Measurement of Small Displacements

$$F_{dr} = K_{flex} (X_2 - X_1)$$

$$K_{gr} = \frac{F_{dr}}{X_1}$$

$$\bar{K}_{gr} = K_{flex} \frac{\sum_1^n \frac{(X_2 - X_1)}{X_1}}{n} = K_{flex} \frac{\sum_1^n \frac{(V_2 - V_1)}{V_1}}{n}$$

Operating Procedure

- Inspect GeoGauge
- Power On
- Select Mode & Poisson's Ratio
- Seat the Foot
 - $\geq 60\%$ Direct Contact
 - Moist Sand Assisted (1/4" to 1/8")
 - Rough & Irregular Surfaces
 - Smooth Hard Surfaces
- Take the Measurement: 75 Sec.
 - 15 Sec. of Noise
 - 60 Sec. of Signal
 - Results Displayed
 - Signal/Noise: $\geq 3/1$ (10 db)
 - Standard Deviation: a Measure of Foot Contact
 - Average Stiffness or Modulus (English or SI)
- Examine the Foot Print
- Save Data

A background image of a construction site. In the foreground, a worker in a white hard hat and orange safety vest stands on the left. Another worker in a white shirt and orange vest is in the center. A third worker in a red and blue shirt is on the right, bent over. In the background, there are large yellow excavators and piles of earth under a cloudy sky.

Performance

Specification

Precision

Bias

Validation & Correlation

Standardization

Specification

- **Stiffness:** 3 (17) to >70 (399) MN/m (klb/in)
- **Young's Modulus:** 26.2 (3.8) to > 607 (88) MPa (kpsi)
- **Poisson's Ratio:** Variable in 0.05 Increments
- **Precision:** Typically 3.9% Coefficient of Variation
- **Bias:** < 1% Coefficient of Variation
- **Depth of Measurement:** 22.9 cm (9 in)
- **Battery Life:** > 1,500 measurements
- **Operating Temperature:** 0°C to 38°C (32°F to 100°F)

Precision

Single Gauge

Date	Site	Material	Typical Stiffness, MN/m		Coeff. Of Var., %		
			Mean	1 σ	Mean	65% Confidence	95% Confidence
8/17/00	Salisbury ByPass	Silty Sand	6.28	0.28	4.08	6.01	7.94
9/20/00	NM 44	Sandy Clay Subgrade*	11.33	0.37	3.31	-	-
10/13/00	16 Vegas Dr.	Sility Clay**	8.86	0.47	5.35	7.17	9.00
10/14/00	16 Vegas Dr.	Full Depth Pavement*	51.37	2.17	4.25	5.66	7.07
10/20/00	170/1270	Graded GAB*	40.20	1.57	3.84	5.21	6.58
10/29/00	Rutters	Fat Clay*	12.74	0.35	2.67	3.13	3.59

* Assisted Seating (moist sand)

** Unprepared ground

- Typical Coefficient Of Variation: 3.9%
- Basis: 3 Gauges, 3 Operators & 470 Measurements

Precision

Multiple Gauges

Date	Site	Material	No. of Measurements	Stiffness, MN/m		Coeff. of Var.
				Mean	1 σ	%
11/7/00	16 Vegas Dr.	Silty Clay* *	12	8.50	0.33	3.89
11/7/00	16 Vegas Dr.	Silty Clay* *	30	9.94	0.39	3.91
11/8/00	16 Vegas Dr.	Full Depth Pavement*	16	44.83	1.72	3.83
11/24/00	16 Vegas Dr.	Silty Clay* *	10	10.06	0.59	5.84

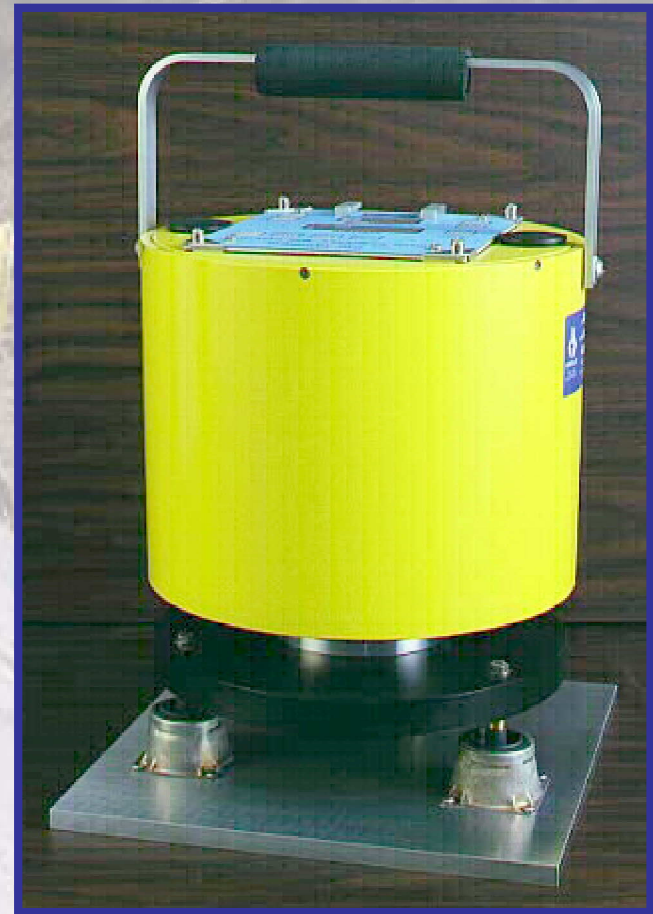
* Assisted Seating (moist sand)

** Unprepared ground

- Statistics Based on Combined Measurements From Both Gauges
- Basis: 2 Gauges, 1 Operator & 68 Measurements

Bias

- **Reference: Moving Mass**
 - **Known Mass: 10 kg (22 lb)**
 - **25 Known Frequencies: 100 to 196 Hz**
 - **Stiffness = $-j\omega^2M$**
- **Coefficient of variation: < 1%**
- **Basis: 100+ Measurements Over 18 Months**



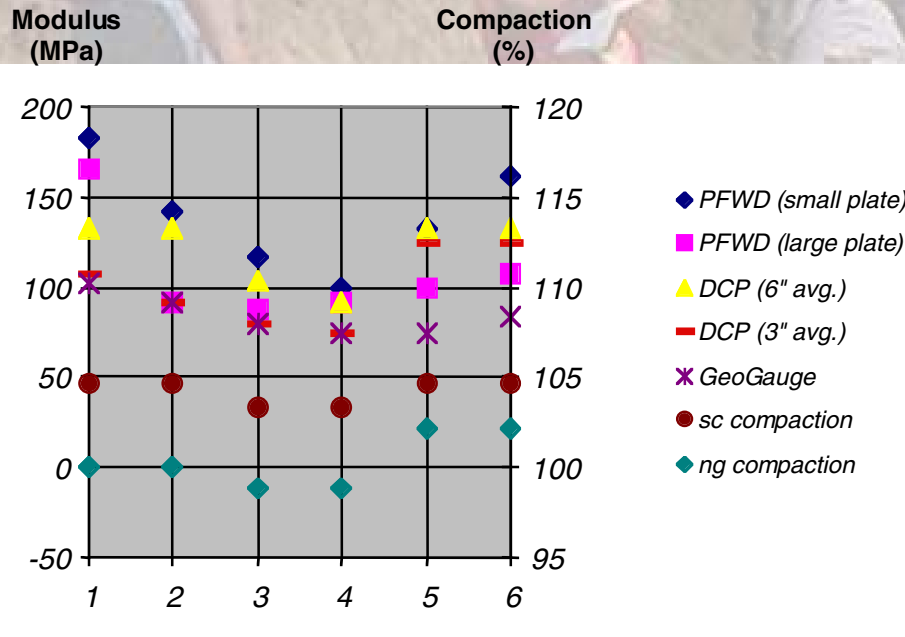
Validation

- Nature of Measurement Validated via CNA Plate Load Tests
- Depth of Measurement, Bias & Effect of Boundaries Validated by Univ. of New Mexico

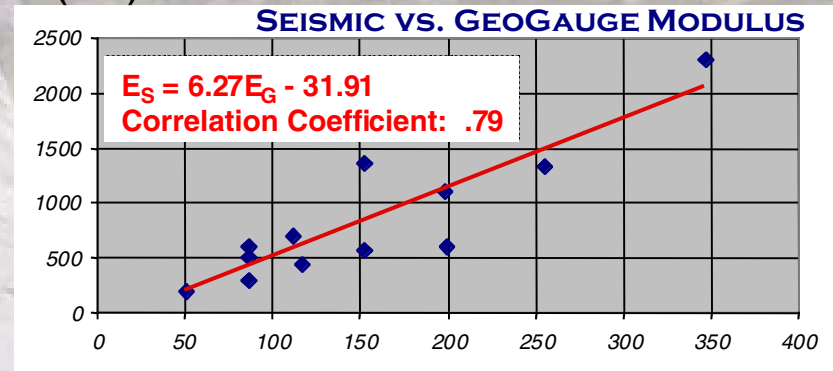
Correlation to Other Moduli

SUBGRADE & BASE MATERIALS IN 6 TXDOT DISTRICTS

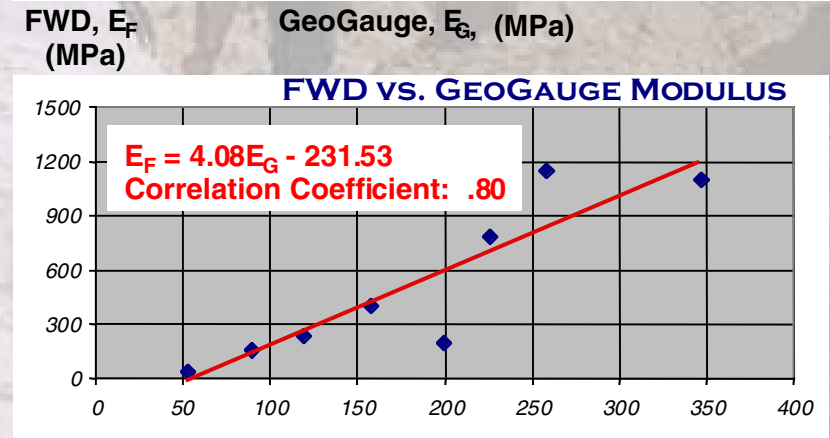
SECTION 17, MN/ROAD



Seismic, E_S
(MPa)



FWD, E_F
(MPa)



13 PAVEMENT SECTIONS
AT 5 MNDOT SITES

GeoGauge, E_G (MPa)

Correlation to Dry Density

DEFINE SEVERAL LINEAR RELATIONSHIPS BETWEEN C AND K/M^{25} FOR GROUPS OF REGIONAL SOIL CLASSES

2

CALCULATE C FROM REGIONAL COMPANION MEASUREMENTS OF STIFFNESS, MOISTURE CONTENT & DRY DENSITY

$$C = (K/m) \left\{ \left[\frac{(\rho_o \rho_D - 1)}{1.2} \right]^2 + 0.3 \right\}$$

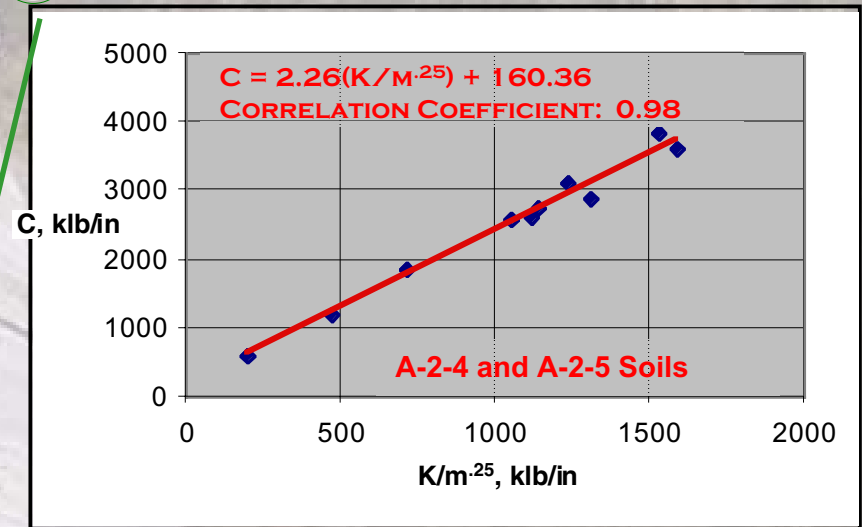
1

ANALYTICAL-EMPIRICAL RELATIONSHIP

$$\rho_D = \frac{\rho_o}{1 + 1.2 \left[\frac{mC}{K} - .3 \right]^2}$$

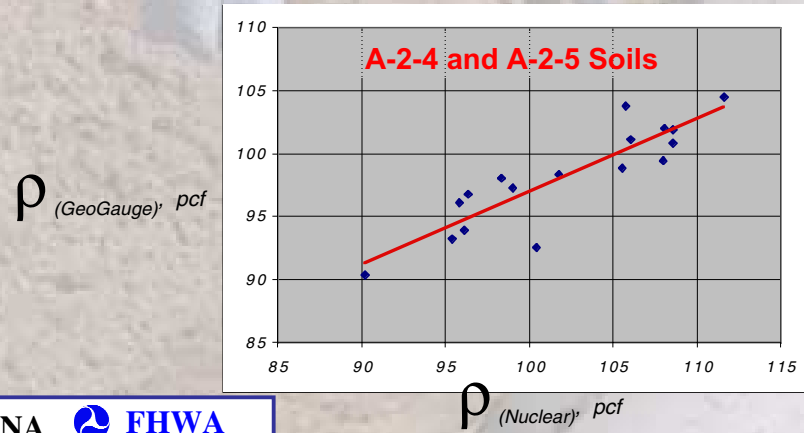
ESTIMATED DENSITY RE MEASURED DENSITY

3



4

FROM MEASUREMENTS OF STIFFNESS & MOISTURE CONTENT AND A CALCULATED C, ESTIMATE DRY DENSITY USING THE SAME ANALYTICAL-EMPIRICAL RELATIONSHIP



$$\rho_{(GEOGAUGE.)} = 0.58(\rho_{(NUC)}) + 39.39$$

CORRELATION COEFFICIENT: 0.78

DATA FROM MODOT, NOVEMBER, '99

Other Correlations

- Resilient Modulus
- Unconfined Compressive Strength
- CBR
- Binkelman Beam
- Static Cone Penetrometer

Standardization

- **ASTM Standard Method**
 - **In-Place Stiffness & Modulus Measurement**
- **1st ASTM D18.08 Ballot: 1 Negative (Resolved)**
- **2nd ASTM D18.08 Ballot: To Be Completed 11/30**
- **ASTM D18 Ballot: Results Expected Early '01**
- **AASHTO Will Review Approved ASTM Standard**

GeoGauge Alternatives

Method: In-Place Stiffness or Modulus	Speed	Simplicity	Depth	Precision	Bias	Production Test*	Non- Destructive Test	Relationship To Density Exists
GeoGauge	1	1	~ 8"	1% to 10%	< 1%	Yes	Yes	Yes
Impact Value (Clegg)	2	2	~ 4"	2% to 20%	?	No	No	?
Field CBR	4	4	~ 20"	?	?	No	No	?
DCP	3	3	Several Feet	?	?	No	No	?
German Plate Load	3	3		?	?	No	No	?
Portable FWD (Loadman)	3	3	~ 10"	?	?	No	No	?
D-SPA	5	5	Several Feet	?	?	No	No	?

Speed: 1 = fastest, 5 = slowest

Simplicity: 1 = Simplest, 5 = Most Complex

? = Quantity Undefined

* Production Test: One that does not delay or interfere with construction

Design History

The Origin of the Technology
Dual Use Technology
Development Approach

- Concept Formulation
- Proof-of-Principle Demonstration
- Commercialization



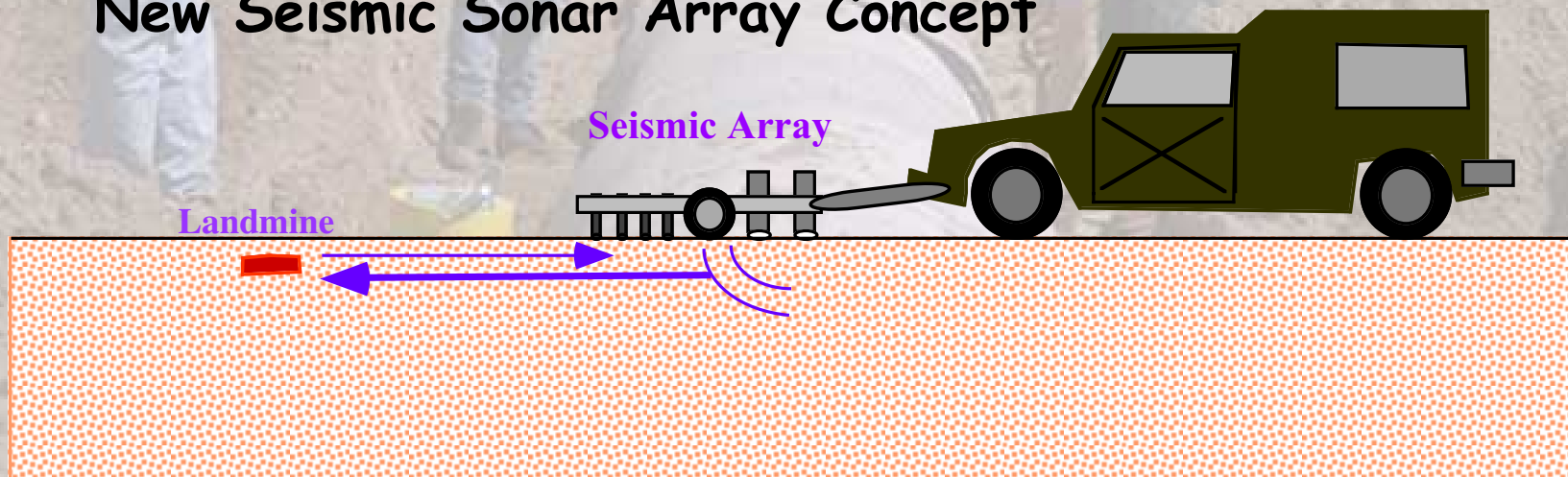
The Origin of The Technology

Seismic Landmine Detection

BBN Seismic Landmine Detection Research

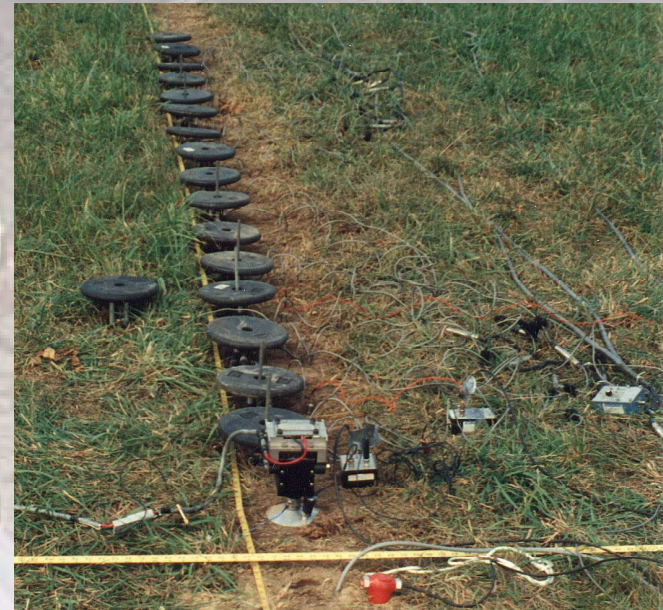
For Army Belvoir R & D Center, '88 to '92

- Goal: Detect Buried, Non-Metallic Mines With Seismic/Acoustic Waves From a Safe Distance
- Feasibility Demonstrated of Mine Detection with New Seismic Sonar Array Concept

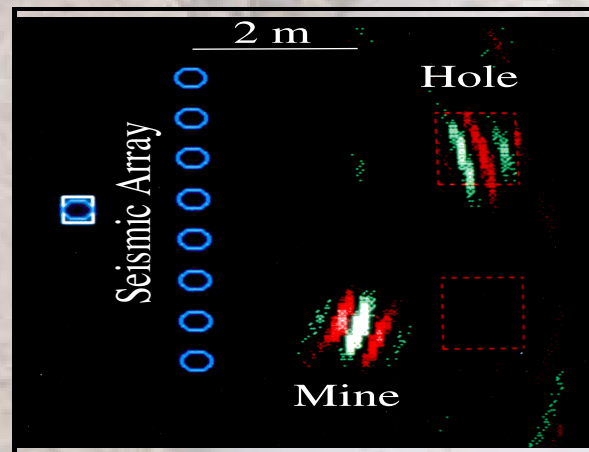


BBN Shallow Soil Seismic/Acoustic Research

- Soil Physics & Measurements
 - Soil Impedance
 - Wave Propagation
- Transducer Coupling Research
- System Development & Displays



BBN Proprietary Weight-biased Geophones and Compact Vibrator Source

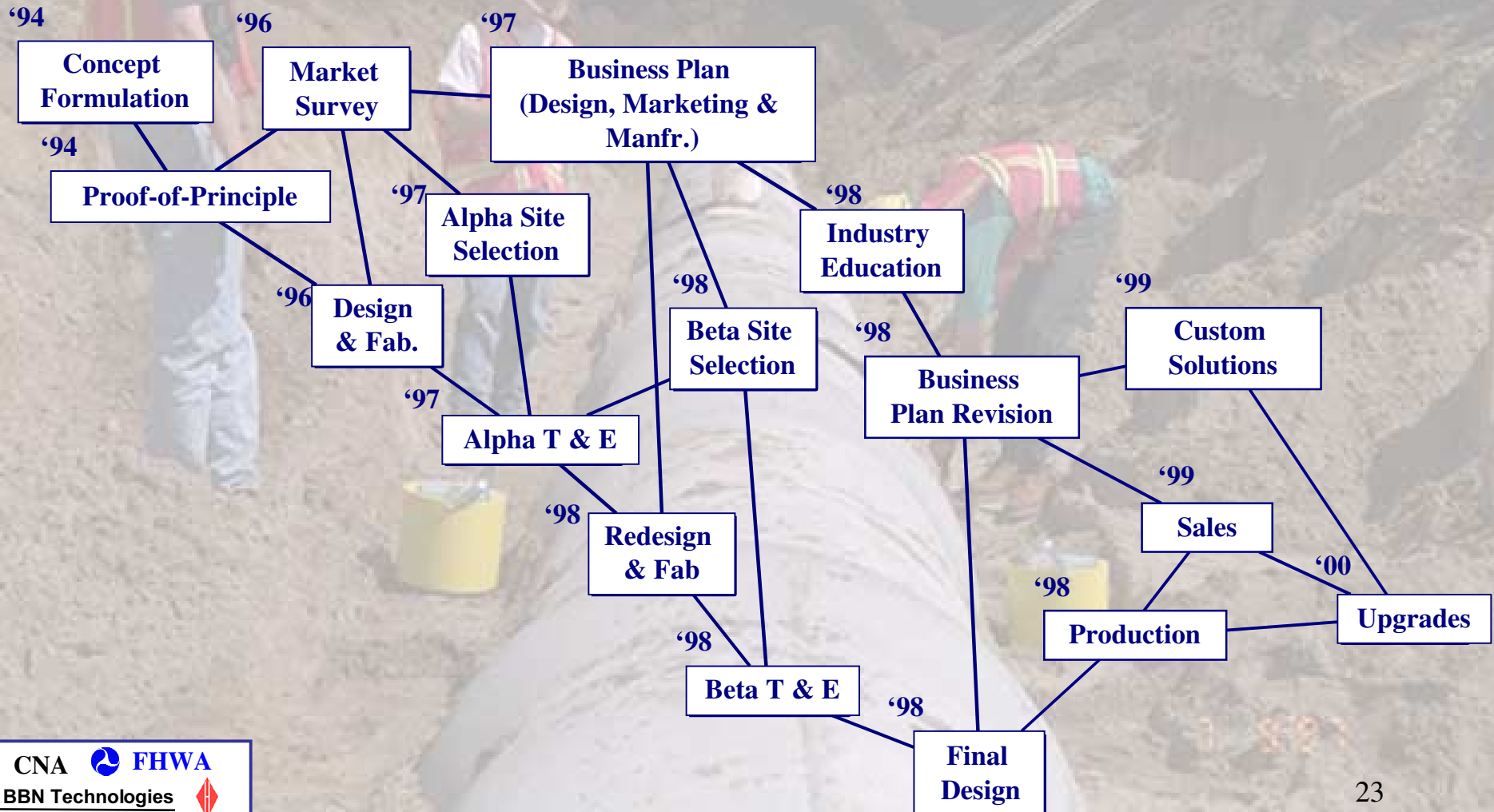


Seismic Sonar Display of Response of Mine

Dual Use Technology

- Logical Transfer to Civil Application
- Transfer via DARPA TRP: '93 to '96
 - BBN, CNA, MTS & MnDOT Team
 - FHWA Designated Program Manager
 - Goal: Use of Stiffness for Evaluating Compaction
- Approach
 - Define Engineering Requirements
 - Define Sales Potential
 - Prototype
 - Commercialize

Development Approach



Concept Formulation

Objectives

- **Dynamically Measure Stiffness**
 - No Absolute Reference Needed
 - Minimize Degradation by Noise & Physical Anomalies
- **Suitable for Widespread Field Use**
 - Materials & Process Control
 - Materials Characterization
- **Real-Time, Statistically Meaningful Sampling**
- **Reasonable Time-to-Market**

Concept Formulation

Selected Attributes

- Accurate Over 3.8 to 28 kpsi min.
- Measurement Depth Typical of Lift Thickness (~8")
- Measurement Period of ~ 1 min.
- Precision: Coefficient of Variation \leq 5%
- Easy to Use: One Person Operation, No Penetration
- Portable: Small & Weighing \leq 30 lb.
- Rugged: As Good or Better Than Current Equip.
- Affordable: \leq \$6,000

Concept Formulation

Design Issues

- Functional Requirements
- Test Signal Design
- Ground Coupling
- Transducers
- Signal Generation & Processing
- Mechanical Design & Packaging
- User Interface
- Calibration & Field Verification
- Basis: Soil Physics From Army & TRP Work

Functional Requirements

- **Overburden Biasing Pressure: 4 to 5 psi**
- **Dynamic Force Level**
 - Sufficient for Signal-to-Noise of 3/1
 - Insufficient to Change Material Properties
- **Dynamic Range to Be Measured**
- **Ambient Ground Vibration: Amplitude & Frequency**

Test Signal Design

- **Frequency Range: 100 to 200 Hz**
 - Adequately High
 - Avoiding Ambient Vibration
 - Allowing Static Coupling of Biasing Pressure
 - Adequately Low
 - Avoiding All But Stiffness In Ground Impedance
 - Avoiding Internal Resonances
 - Adequately Broad
 - Enhancing Signal-to-Noise
 - Avoid Resonances From Physical Anomalies
- **Wave Form**
 - Stepped Steady-State
 - Duration: 2 Sec.

Ground Coupling

- **Foot Geometry: Ring Shaped Plate**
 - Depth of Measurement
 - Quality of Soil Contact (Coupling)
- **Foot Properties**
 - Low Mass
 - High Stiffness
- **Static Biasing Weight: 22 lb.**
 - Quality of Soil Contact (Coupling)
 - Meaningful Overburden Pressure
- **Resilient Mounts**
 - Dynamic Decoupling
 - Physical Stability

Transducers

Trade-Offs

- **Shaker**
 - Cost
 - Output Level, Bandwidth, Linearity, Ruggedness
- **Motion & Force Sensors**
 - Cost
 - Sensitivity, Noise, Dynamic Range, Bandwidth, Linearity, ...
- **Mass Loaded Geophones Selected**
 - Statically Coupled to Ground
 - Dynamically Decoupled From Ground

Signal Generation & Processing

- **Hardware Architecture**
 - Analog - Digital Marriage
- **Algorithms**
- **Numerical Values of Processing Parameters**
- **Hardware Devices**
 - Cost
 - Accuracy & Precision, Dynamic Range, Power, ...
- **Hardware Layout & Packaging**
 - Discrete vs. Surface Mount
- **Software**

Mechanical Design & Packaging

- **Structural Integrity**
- **Manufacturable, Testable, Repairable & Upgradeable**
 - Modularity
- **Consistency With Function**
 - Stiffness & Mass
 - Frequency Response
- **Survivability: Mechanical & Environmental**

User Interface

- Cost
- Off-the-Shelf
- Presets vs. Operator Control
- Information: Displayed & Stored
- Engineering Units

Calibration & Field Verification

- **Method**
 - Standard Stiffness vs. Standard Mass
 - Factory Cal. vs. Field Verification
- **Calibration Algorithm**
 - Estimation of Gauge Stiffness
- **Standard Mass Implementation**
 - **Factory Calibration: < 1% Coeff. of Variation**
 - Value of Mass : 22 lb.
 - Fixture: Gauge Bolted to Isolated Mass
 - **Field Verification: ~ 5% Coeff. of Variation**
 - Value of Mass : 22 lb.
 - Fixture: Mass Bolted & Hung From Gauge

A photograph of a construction site. In the foreground, a large, cylindrical object wrapped in white plastic is being moved or positioned. Several workers in safety vests and hard hats are visible. In the background, there are large excavators and piles of earth under a cloudy sky.

Proof-of-Principle: '94

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Proof-of-Principle (1994)

- Partners (2 agencies, 2 contractors)
 - Minnesota DOT
 - Metropolitan (Mpls/St. Paul) Council Env. Services
 - Johnson Brothers Corporation
 - Lametti and Sons
- Technical
 - Does it work / What do we measure?
 - What are the “preferred” measurement features?
- Market Forces



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1994 Technical Proof-of-Principle

- Ground coupling
- Foot design
- Reliability & repeatability
- Densification during testing
- Machine weight
- Soil moisture content
- Signal to noise ratio / drive level
- Depth of measurement
- Frequency range / frequency dependence



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Summary of Minnesota Field Testing

Site	Description	Cooperative Partners	Soil Description
Blaine Interceptor	deep interceptor sewer, constructed by trench and fill	MCWWS	Recompacted trench backfill at surface; deep natural & recompacted soil
Mendota TH 110, 55 & 13	large highway project, testing done on or near eastbound TH 110 east of TH 55 crossover	MnDOT JBC	Roadway subgrade; dense natural soil
Inver Grove Heights TH 55 & 3	large highway project, testing done on an entrance ramp to westbound TH 55	MnDOT	Roadway subgrade



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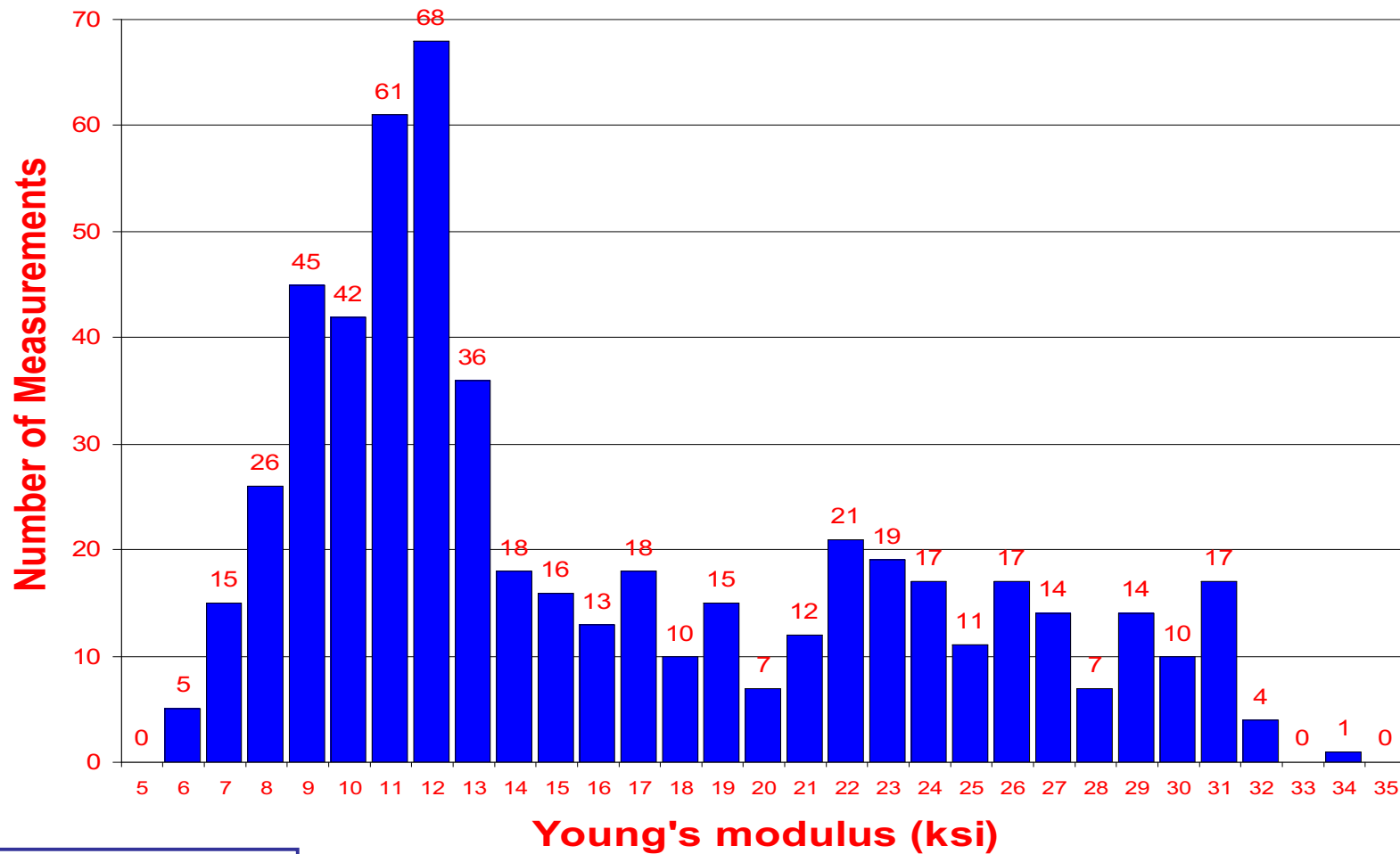
Summary of Field Testing

Site	Locations	Stiffness Measurements	Background Noise Datasets
Massachusetts	3	200	na
Blaine Interceptor	22	188	12
Mendota TH 110, 55 & 13	36	321	7
Inver Grove Heights TH 55 & 3	14	50	4



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Distribution of Field Data



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Proof-of-Principle Apparatus



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Proof-of-Principle Apparatus (close-up)



CNA		FHWA
BBN Technologies		
	verizon	

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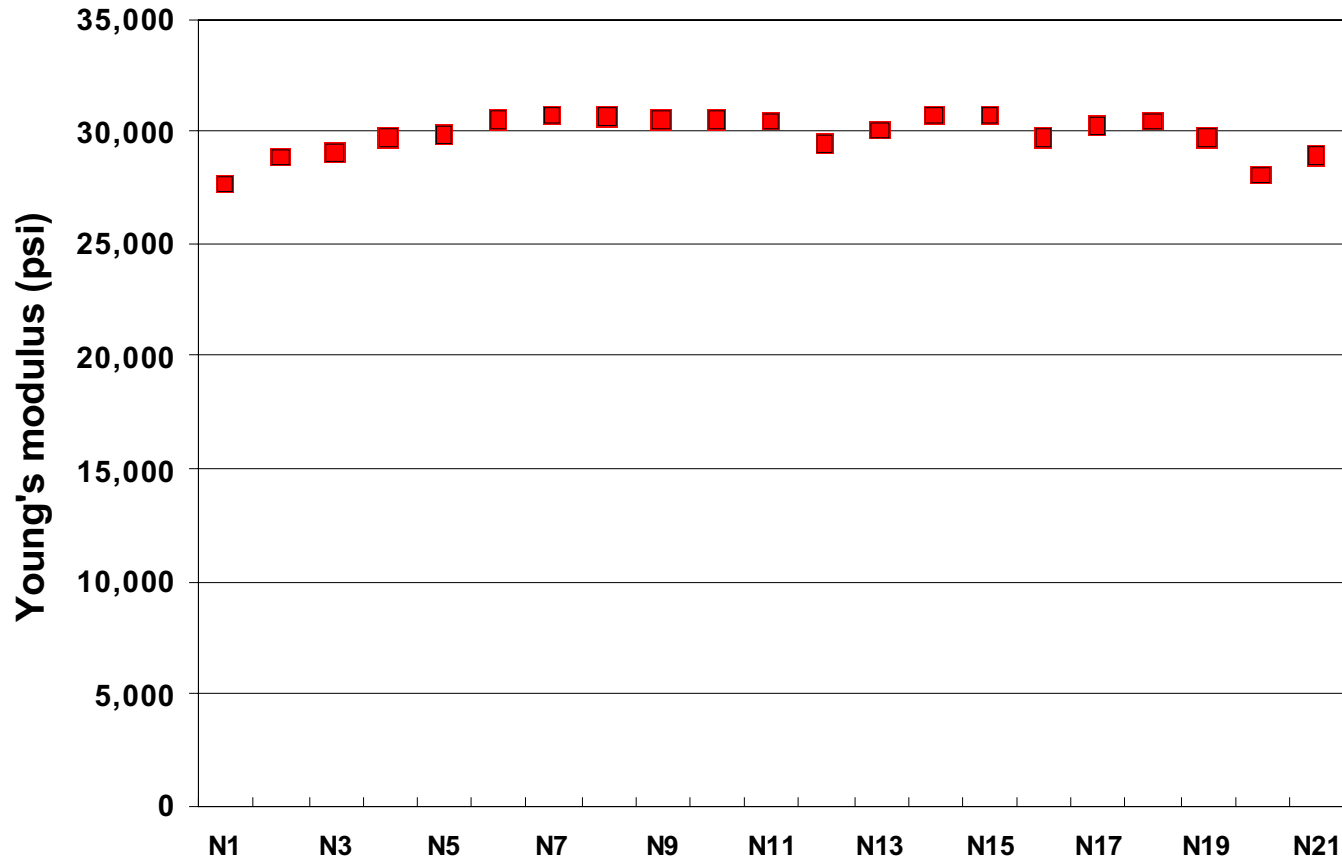
Ground Coupling & Foot Design



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Repeatability, Densification, Coupling

Mendota T.H. 110, 55 & 13 - Location N



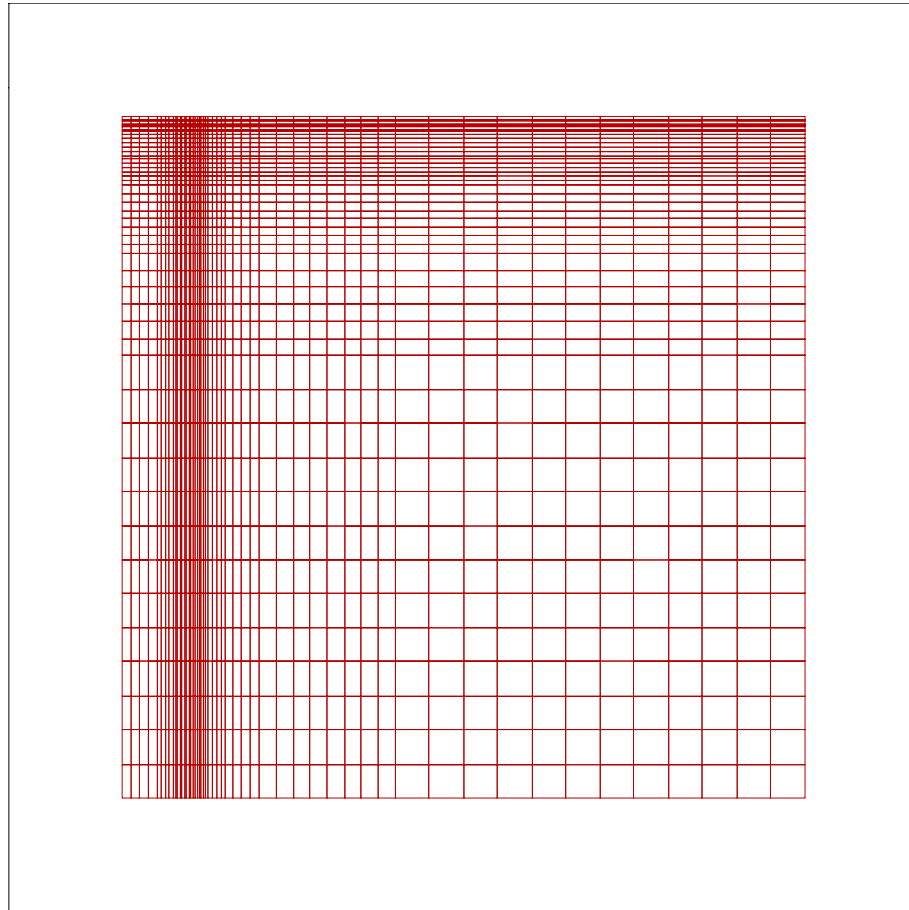
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Modeling

FLAC (Version 3.40)

LEGEND

24-Nov-0 15:44
step 35600



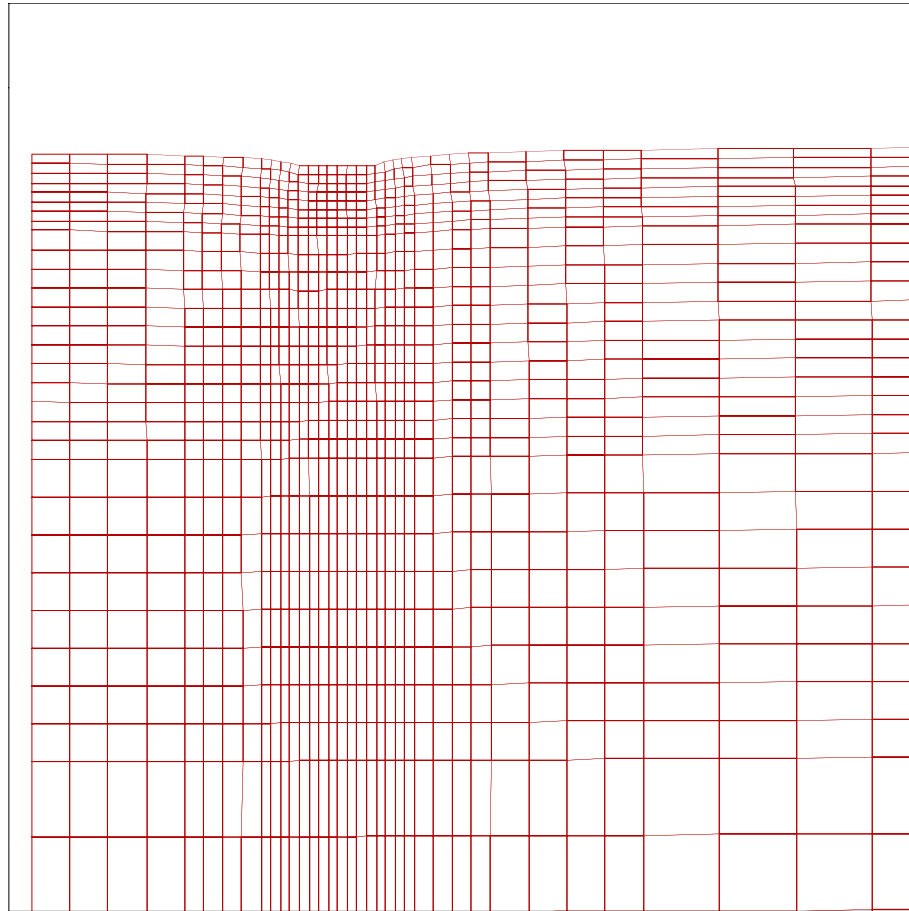
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Displacements

FLAC (Version 3.40)

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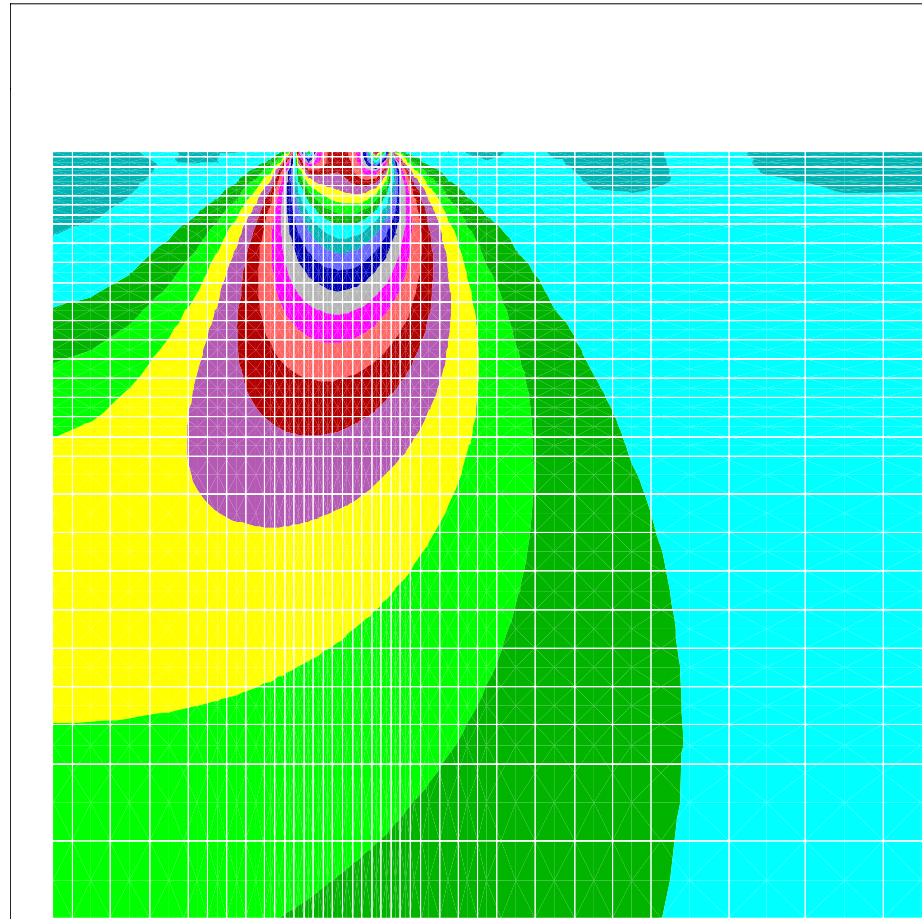
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Stresses

FLAC (Version 3.40)

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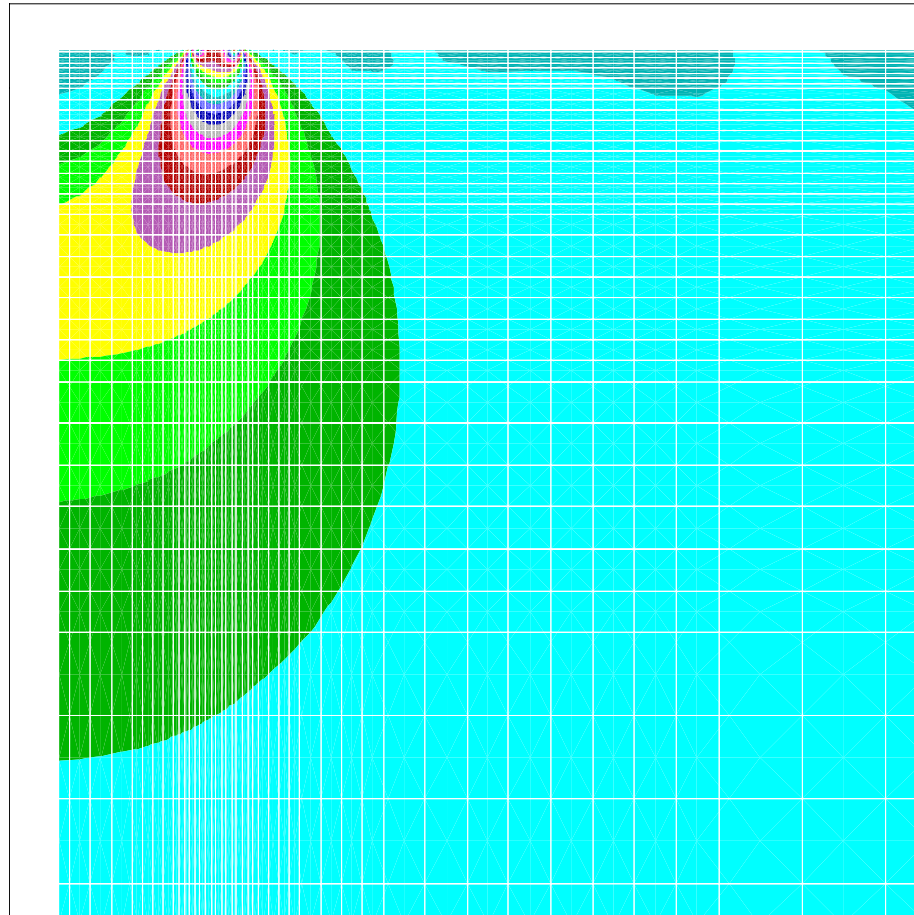
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Stresses

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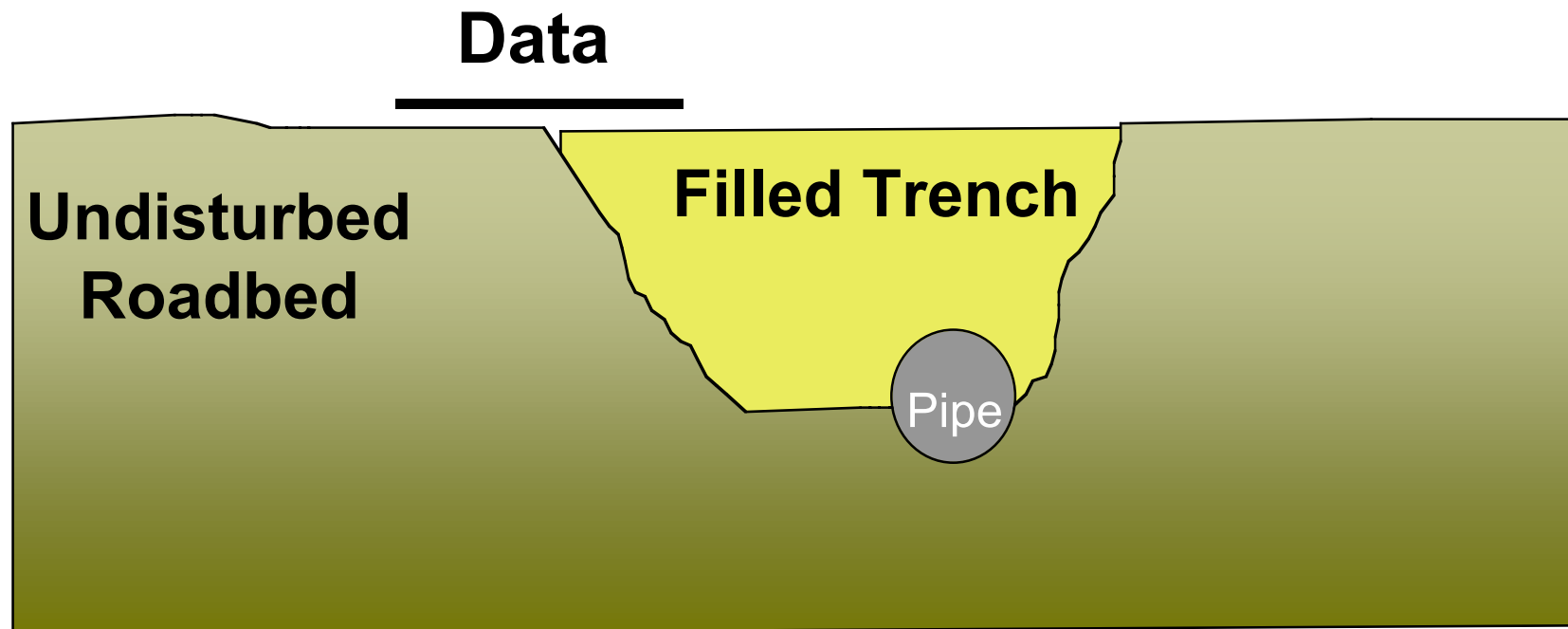
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Backfilled Trench Example



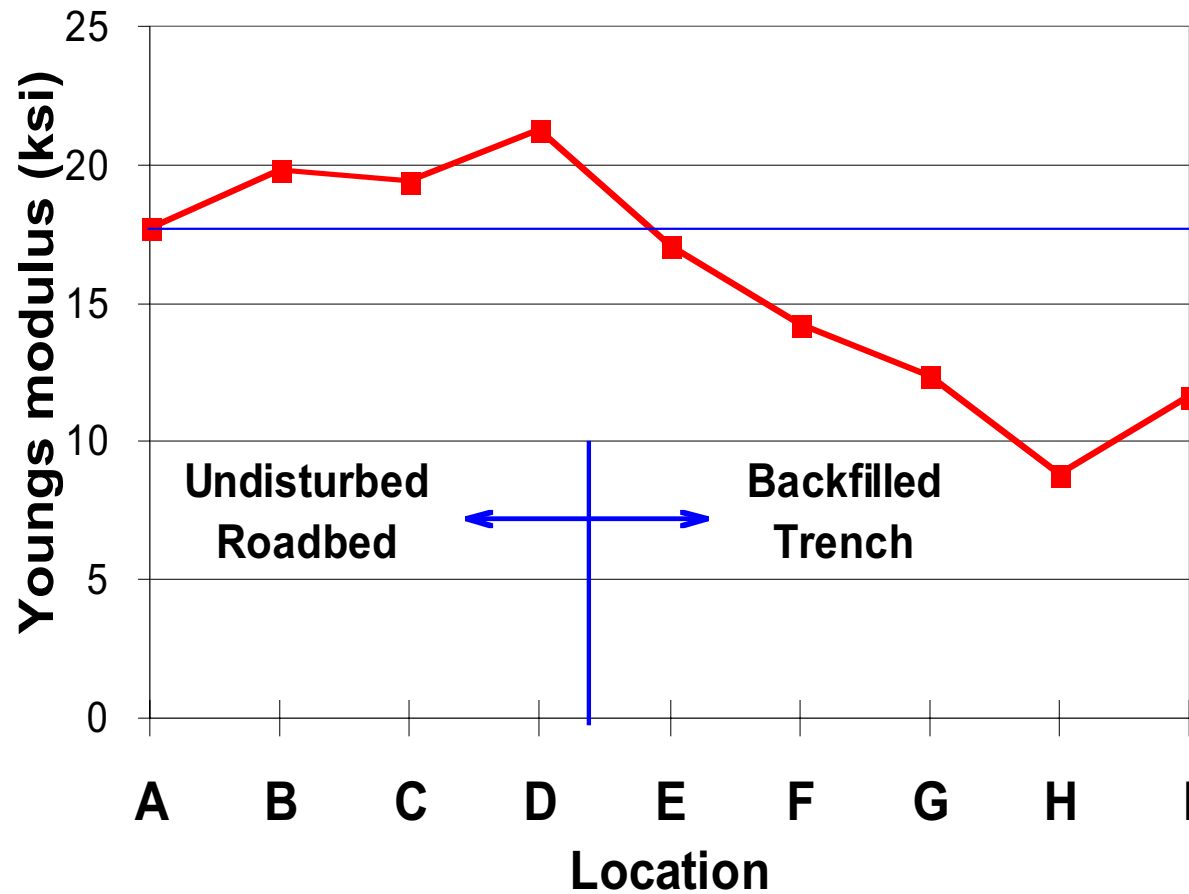
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Backfilled Trench Example



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Backfilled Trench Example



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Market Driving Forces

Benefits

Reduced Compaction Effort



**Superior, More Uniform
Soil Foundations**



**Better Engineering Design
Data**



Outcomes

Contractor Profitability



Reduced Acquisition Cost

Better Quality Structures

Increased Service Life



**Reduced Owner
Life-Cycle Cost**

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Industry Feedback

- Overcompaction & undercompaction occur
- Uniform compaction is desirable
- Experienced inspectors vs. measurements
- Agency standards & acceptance
- Documented results
- Demonstration projects
- Process control concepts



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Commercialization

Design Validation: '97 to '98

Marketing: '96 to '00

Production: '98 to '00

Design Validation

- **Alpha**
 - Field Trials: MN, NY & TX
 - Construction Noise: Freq. Shift & Improved Filtering
 - Calibration: Soil vs. Elastomer vs. Mass
 - Relationship Between Density & Modulus
- **Beta**
 - Field Trials: MN, TX, NC, FL, OH, CA, NJ & MO
 - Usability & Reliability
 - Manufacturing & Test Methods Development
 - Establish Precision & Bias
- **Standards Development**

Marketing

- **Market Survey**
- **Business Plan Development & Evolution**
- **Alpha & Beta Site Selection & Lessons Learned**
- **Education: The Value of Stiffness & Modulus**
- **Custom Solutions: Realizing Immediate Benefits**
- **Market Driven Product Improvements**

Production

- Manufacturing Plan: 10s to 100s annually
- Design Manufacturability
- Material Sourcing
- Manufacturing, QA & QC Methods
- Training
- Facilities



Enabling the Benefits of Stiffness & Modulus Today

Control of the Compaction Process
Mitigating the Risk of Pavement Failure
Control of Stabilized Fill Quality

CNA  FHWA

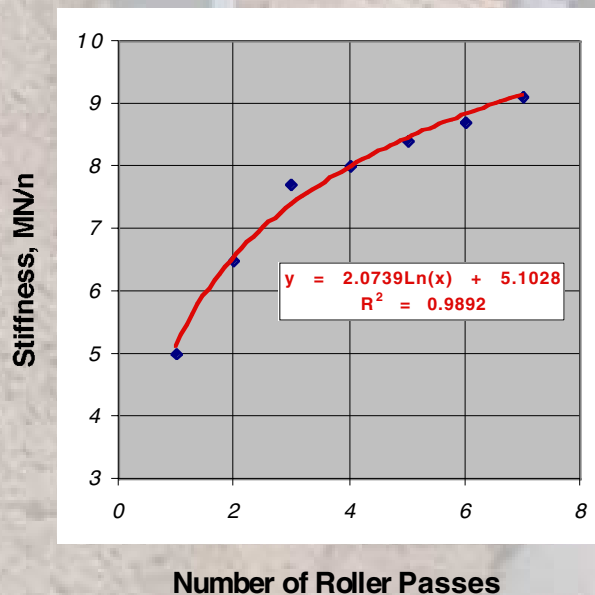
BBN Technologies 

 verizon

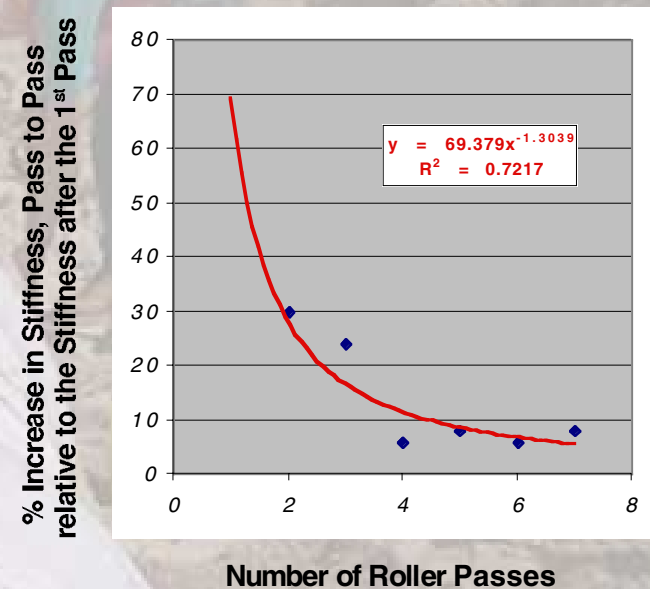
 HUMBOLDT

Control of the Compaction Process

- Compaction of A Layer Is Only As Good As the Supporting Material Will Allow
- Directly Measure Compaction (Rate of Increase in Stiffness) As a Function of Effort
- When the Rate Is Approx. Constant, the Compaction Is Optimized
- ~ 30% Reduction in Compactive Effort Possible



COMPACTION OF 2" OF HMA
MANGUM ASPHALT, INC.
JUNE, 2000

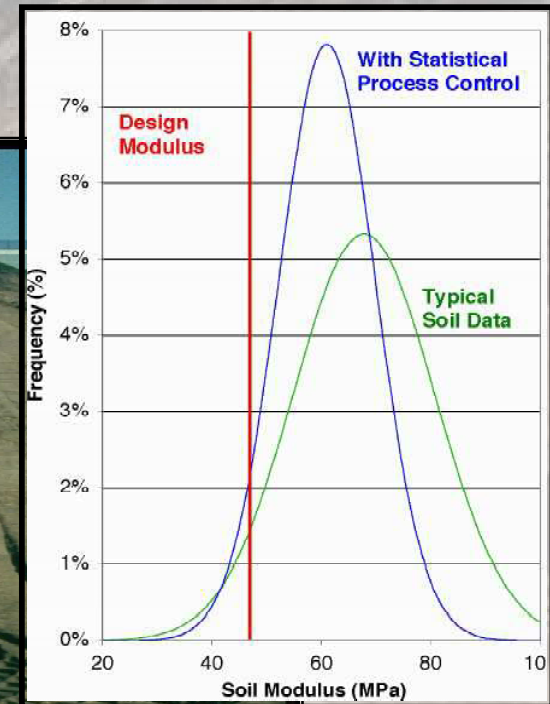
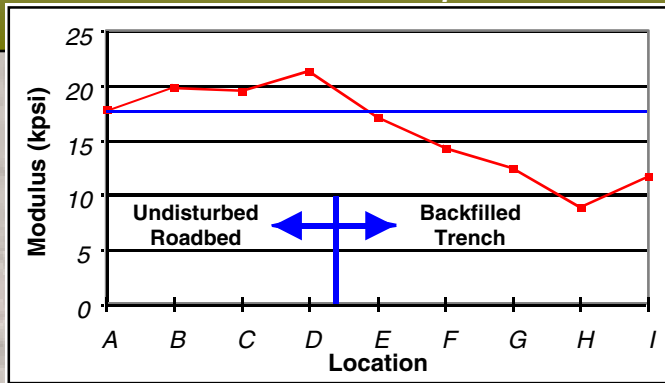


OPTIMUM COMPACTION WITH MINIMUM EFFORT

Mitigating the Risk of Pavement Failure

More Uniform Stiffness = More Time Between Failures

Data

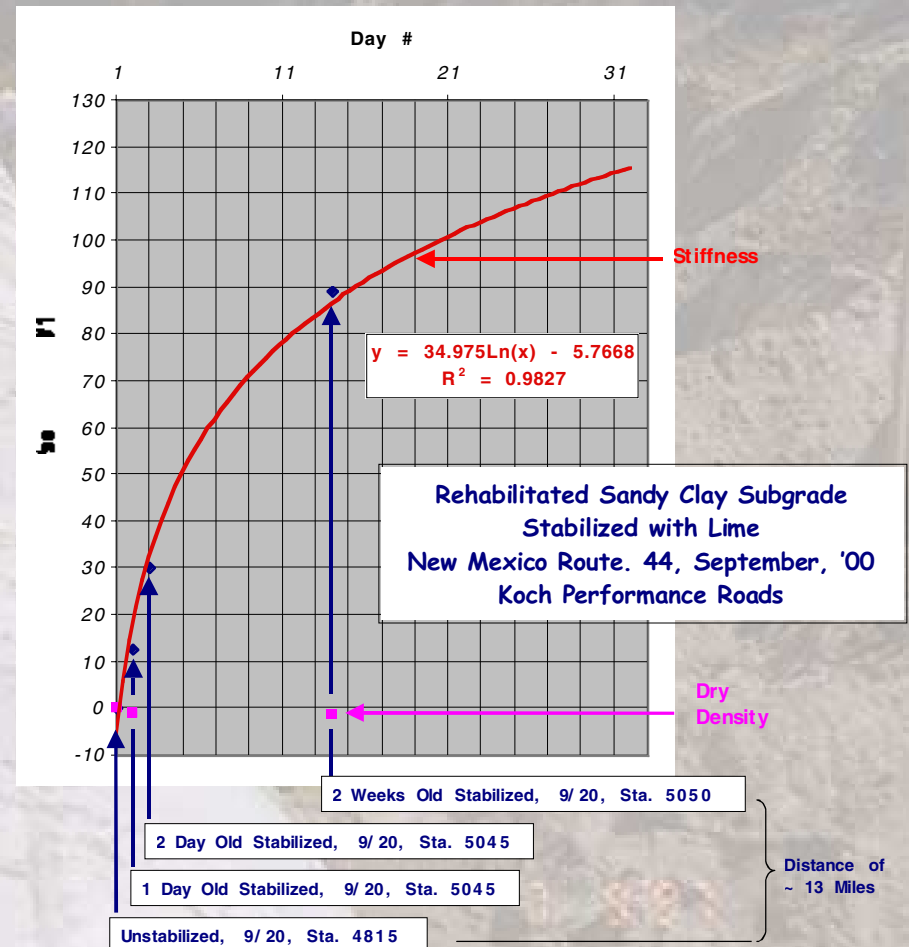


- Sharp Stiffness Changes = Near Term Failures
- Experience Is Indicating:
 - + 50% Stiffness Tolerance, Fewer Near Term Failures
 - + 25% Stiffness Tolerance, Fewer Long Term Failures

Control of Stabilized Fill Quality

- “Is the Fill Hard Enough?”
- “Has Rain Inhibited Stabilization?”
- “Can I Customize Stabilization?”
- GeoGauge Can Enable:
 - Monitoring of Material Cure Rate
 - Direct Measurement of Material Modulus
 - Laboratory Design of Custom Mixes & Determination of Indexes for Evaluating Construction
- GeoGauge Specified By USAF for Runway Infield Stabilization
 - Used to Estimate Increases in CBR

Evaluation of Stabilization



Some Other Applications

- Specification Development
- Mechanistic Design Validation
- Buried Structures QC
- Utility Back-Fills QC
- Determination of HMA "Tender Zone"
- Evaluation of Controlled Low Strength Materials
- Quantification of Soil-Cement Micro-Cracking
- Cold Mix Asphalt QC